CRITICALITY ANALYSIS OF URANIUM STORAGE FACILITY WITH FORMATION RACKS

Sri Kuntjoro Center for Technology and Nuclear Reactor Safety - BATAN PUSPIPTEK, Building 80, Setu, Tangerang Selatan 15310

e-mail: srikuncoro@batan.go.id, telp. : 021-7560912, fax: 021-7560913 Diterima editor: 14 Februari 2017 Diperbaiki: 1 Maret 2017 Disetujui untuk publikasi: 2 Maret 2017

ABSTRACT

CRITICALITY ANALYSIS OF URANIUM STORAGE FACILITY WITH FORMATION RACKS. Uranium materials are needed for the uranium fuel production of research reactors and radioisotope. Before the uranium material is used, it is stored in the storage facility. One of the prerequisites for uranium material storage facilities is that it must be in the sub-critical condition. The purpose of this study is to analyze the criticality condition of uranium material storage facility located in PT. Inuki (Persero) and to ensure that the criticality condition is always in sub-critical state. Criticality analysis was performed using MCNP-5 program to determine the level of criticality of the three uranium material storage facilities 1 and 2, three scenarios of container on the storage rack formations were considered. Meanwhile, for analysing the storage facility 3, one scenario was considered. The results confirm that all strorages at initial condition and after adding storage racks formation were still in sub-critical condition (k-eff<1). These results are then used as the basis for the uranium materials management. It is also used as a basis for issuing an operational license by the nuclear energy regulatory body (BAPETEN).

Key words : criticality, uranium storage facility, k-eff

ABSTRAK

ANALISIS KRITIKALITAS DI FASILITAS PENYIMPANAN BAHAN URANIUM DENGAN FORMASI PENGATURAN RAK. Bahan uranium dibutuhkan untuk produksi bahan bakar reaktor penelitian dan radioisotop. Bahan uranium sebelum digunakan terlebih dahulu disimpan pada fasilitas penyimpanan. Salah satu prasvarat fasilitas penyimpanan bahan uranium adalah fasilitas tersebut harus dalam kondisi sub-kritis. Bila kondisi kritis terjadi mengakibatkan proses fissi pada bahan uranium tidak terkendali, sehingga akan menimbulkan suhu yang sangat tinggi. Tujuan dari penelitian ini adalah untuk menganalisa kondisi kritikalitas dari fasilitas penyimpanan bahan uranium yang berada di PT. INUKI (Persero) untuk menjamin fasilitas tersebut dalam kondisi sub-kritis. Analisis kritikalitas dilakukan menggunakan program MCNP-5 untuk mengetahui tingkat kritikalitas dari tiga fasilitas penyimpanan bahan uranium untuk kondisi awal dan kondisi setelah ditambahkan rak penyimpanan. Untuk fasilitas penyimpanan 1 dan 2 dibuat tiga skenario pengaturan container pada rak penyimpanan, sedangkan pada fasilitas penyimpanan 3 dilakukan 1 skenario. Hasil ini menunjukkan seluruh fasilitas penyimpanan pada kondisi awal dan setelah ditambah rak penyimpanan dalam kondisi sub-kritis (k-eff ≤ 1). Hasil tersebut selanjutnya dipergunakan sebagai dasar untuk menyusun manejemen pengelolaan bahan uranium. Selain itu juga digunakan sebagai dasar untuk pembuatan ijin dari badan pengawas (BAPETEN).

Kata Kunci : kritikalitas, fasilitas penyimpanan berbahan uranium, k-eff

INTRODUCTION

Radioisotope and fuel production require low enriched uranium (LEU). Uranium materials require storage facility prior to use. Storages of uranium materials have prerequisites, among others, where it should be in a sub-critical condition. These prerequisites must be satisfied since if critical conditions occur, it will cause the uncontrolled fission on uranium material. As a result, a high heat is generated in the uranium material, which could melt the uranium material itself. Melting of uranium materials will lead to the release of fission products in the form of radioactive materials into the environment and can be hazardous to people as well as the environment.

Criticality calculations are performed at nuclear facilities, fuel storage, and storage of uranium materials. The analysis was performed to ensure existing facilities in sub-critical condition to avoid uncontrolled fission reactions and high temperature in the facilities. Criticality calculations can be done using a variety of computer program such as MCNP-5 computer code, which is based on Monte Carlo method [1]. Critical analysis on various cases have been done by previous investigators, for example, on various geometry fuel arrangement by Doddy Kastanya [2], TRIGA Mark II reactor first criticality by D. Alloni et.al [3], as well as the fuel storage facility at the TRIGA Mark II research reactor by Loren R Metthew [4]. It also has been carried out for criticality calculation of high temperature reactors, research reactors and other criticality problems. Criticality calculations for high temperature power reactor as for the pebble and HTR reactor criticality has been conducted by Meng-Jen W, et al, Meng-Jen W, et al, Evi Setiawati, at al and several other researchers [5–11]. For the calculation of criticality at research reactor as in the Ghana LEU research reactor has been conducted by Henry Cecil O [12]. In addition, the calculation of the other criticality calculations for effect of difference nuclear library, influence of normalization flux and influence of geometry models have been done by R. Mosteller et al, Gasper Zerovnik and Christopher R. Hughes, et al respectively [13–15].

Criticality research has been done around the reactors and spent fuel storage facility and no one has been done on uranium material storage facilities. The purpose of this study was to analyse the criticality condition of the uranium material storage facility in the PT. INUKI (Persero). This study was conducted to determine the criticality condition of the storage facilities 1, 2 and 3 at the initial conditions and at the condition with additional storage racks. At the storage facility 1 and 2, which contain storage racks, analysis was made in three scenarios, while for the storage facility 3 was made just one scenario.

The first step in this analysis is to make the cell calculation model for uranium material that will be stored in a storage facility. Furthermore, the density atom calculations are performed for all material in the cell calculation. Atomic density calculations are also done for all material in the system calculation. The Atomic density obtained in the cell and system model are used as an input to the MCNP-5 codes. Both of these inputs are used in the calculation of criticality of the system storage facility for the current condition and the condition after storage racks are installed. Further analysis is to determine the level of criticality of the system of fuel storage facility for the current condition after storage racks. Results are used for the fuel management as well as the basis for uranium materials management license from the regulatory body (BAPETEN/Indonesia Nuclear Energy Regulatory Agency)

THEORY

MNCP-5 Computer Program

Criticality analysis can be performed using a MCNP-5 program package. MCNP-5 is a computer program used to analyze the particle flux by the Monte Carlo method. Monte Carlo method is a method of solving the problem of neutron transport in a way to simulate the trail of particles to follow the lead of the particles since the "birth" followed step by step in a medium that has been defined until the neutron particles are diminished from the medium, followed by other particles sequentially. For neutron flux calculation, a library of cross-section for the medium

through which the particles neutrons (σ 1, σ 2, σ 3) has been available in the package, while the probability of particles neutrons interacting medium that is passed is determined randomly by plant random number (random number generator), for it takes the density of the medium as an the program. The number of neutron particle that passes through a medium is calculated (scored), the number of neutrons is the neutron flux at the point observed[1].

Precision of the calculation packages of MCNP-5 program is determined by three parameters, namely;

a. The error relative to the 1-sigma standard deviation, which is defined as:

$$R = \frac{S_{\bar{x}}}{\bar{x}} \tag{1}$$

with $S_{\bar{x}}$ is the standard deviation, \bar{x} is the price of the average flux count. Calculations with location detection point (point detector) is considered to meet the criteria if R < 0,05.

b. Variance of Variance (VOV), which is defined as;:

$$VOV = \frac{\sum_{i=1}^{C} (x_i - \bar{x})^2}{[\sum_{i=1}^{C} (x_i - \bar{x})^2]^2} = \frac{1}{C}$$
(2)

where C is a count of particles. Calculations with accuracy MVNP considered eligible if the VOV value is < 0,1.

c. Figure of Merit (FOM), which is defined as;:

$$FOM = \frac{1}{RT}$$
(3)

where T is simulation time. The results of computer simulations considered carefully when FOM is relatively constant value for each sequence capture particles traced. If the parameter is not reached, then calculation is repeated by adding traced neutron or computer calculation time until the parameter value is reached.

d. Geometry and Cross-section data

Input data for MCNP-5 code are comprised of the geometry specification and the cross-section data. The required data of the geometry specification involves of the 2 or 3 dimensional geometric shapes, the volume of material composition and also the material mass. For the cross-section data require the material composition, the energy for neutron fission reaction and the cross-section data library as a function of energy

Determination of the mass fraction and volume fraction and atomic densitiy of chemical elements of a material

The mass, mass fraction, volume fraction and atomic density of a chemical element are required as inputs to the MCNP-5 computer program. The chemical element is a medium through which a neutron particle. It is an observation point where there is a trail of neutron from birth until it disappeared from the media. To determine the mass fraction and the volume fraction, the atomic density building blocks of matter is required. The material volume data is also required. The formula for determining the mass fraction, volume fraction and the atomic density are as follows.

For an example, the material of UO₂ has a density $\rho(uo_2)$ (g/cm³), with enrichment of ω % and Molar weigh of UO₂, U, U-235, U-238 and Oxigen are M(UO₂), M(U), M(U-235), M(U-238) and M(O) respectively, then the steps are:

- Determining the mass of material (gram)

$$Mass of U = \frac{\omega x M(U - 235) + (1 - \omega) x M(U - 238)}{\omega x M(U - 235) + (1 - \omega) x M(U - 238) + 2 X M(O)} x mas of UO_2$$

Mass of Oxygen =
$$\frac{M(U)}{\omega x M(U - 235) + (1 - \omega) x M(U - 238) + 2 X M(O)} x \text{ mas of } UO_2$$
(5)
mass of $U - 235 = \omega x \text{ Mass of } U$

M(O)

(4)

mass of
$$U - 238 = (1 - \omega) \times \text{Mass of U}$$
 (7)

- Determining the mass fraction and volume fraction of material
$$mass of II - 235$$
 (8)

mass fraction of
$$U - 235 = \frac{Mass of U}{Mass of UO_2}$$
 (6)

mass fraction of
$$U - 238 = \frac{mass of U - 238}{Mass of UO_2}$$
 (9)

Volume fraction of U =
$$\frac{\frac{Mass of U}{density of U}}{\frac{Mass of UO_2}{density of UO_2}}$$
(10)

Volume fraction of Oksigen =
$$1 - V$$
olume fraction of U (11)

- Determining the atomic density (atom/cm³)

Number density of U - 235 =
$$\omega x \rho(uo2) / M(U - 235) x(\frac{M(U)}{M(UO_2)})$$
 (12)

Number density of U - 238 =
$$\omega x \rho(uo2) / M(U - 238) x(\frac{M(U)}{M(UO_2)})$$
 (13)

Number density of Oxygen =
$$\omega x \rho(uo2) / M(0) x(\frac{M(U)}{M(UO_2)})$$
 (14)

METHODOLOGY

CELL MODEL FOR URANIUM

The uranium cell consists of two types of cylindrical containers, which are made of uranium, of which 1 piece of container is loaded with natural UO_2 with mass of 1.273 kg and 1 piece of container loaded with depleted uranium metal with mass of 3.576 kg. Each container has a diameter of 14 cm and 17 cm, respectively.

SYSTEM MODEL FOR THREE STORAGE FACILITIES

System Model for Current Storage Facility

Sorage Facility 1

Storage facility 1 is a room measuring of 3.36 m long, 3.10 m wide and 5.25 m high. Storage facility 1 in the current condition contains 10 pieces of containers loaded with natural UO2 each of mass 1.273 kg and 10 containers loaded with depleted uranium metal each of mass 3.576 kg. Each container has a diameter of 14 cm and 17 cm [16]. Each container has designed of 30 cm distance from each other. The container is made of plastic.

Storage Facility 2

Storage facility 2 is a room measuring of 3.36 m long, 3.10 m wide and 5.25 m high. The storage facility 2 currently contains five pieces of container loaded with natural UO2 each of mass 0.106 kg and 5 pieces of container loaded with a mass of 18.418 kg UF4. Each container has a diameter of 30 cm and 34 cm high [16]. Each container has been designed to have a space of 70 cm from each other. The container is made of iron.

Storage Facility 3

The storage facility 3 is a room measuring of 3.36 m long, 3.10 m wide and 5.25 m high. The condition of storage facility 3 currently contains 20 pieces of container-laden natural UCaF2 each of mass 2.373 kg with 19.75% enrichment; and 20 pieces of metal container-laden with uranium enrichment, 19.75% enrichment with the mass of 7.111 kg. Model calculations can be seen in Figure 4. Each container has a diameter of 10 cm and 23 cm high [16]. Each container has been designed of a space 30 cm from each other. The container is made of iron.

System Model with Storage Racks

Storage Facility 1

Storage facility 1 was designed to contain 2 storage racks separated by a distance of 1 m. Each storage rack consists of 3 levels of shelves.

The ground floor of each shelf contains 2×4 units of container and each container of 30 cm diameter and 70 cm high. The container which is located on the ground floor, on the first shelf and the second shelf were loaded with UCaF2 with mass of 2.373 kg with 19.75% enrichment and 7.111 kg uranium metal with 19.75% enrichment [16]. Each container has designed of 50 cm apart from each other.

Furthermore, every shelf level consists of 3 x 6 containers. Containers at all shelves are 14 cm in diameter and 17 cm high. Each container is separated by 39.5 cm. All containers made of iron.

a. The first scenario

- The ground floor contains 2x4 containers, 4 containers were each loaded with UCaF₂ mass of 2.373 kg with 19.75% enrichment, and 4 other containers each loaded with metal Uranium mass of 7.111 kg with 19.75% enrichment.
- The first rack and a second rack each consisting of three shelves. The first to third shelves, where contain of 6 containers each. The entire racks contain of 36 containers with the mass of each container was 1.273 kg of natural UO₂.

b. The second scenario

- The ground floor contains 2x4 containers, 4 containers each loaded with 2.373 kg UCaF₂ with 19.75% enrichment, and 4 other containers each loaded with 7.111 kg metal Uranium with 19.75% enrichment.
- The first and the second rack consist of three shelves. All shelves contain 6 containers each. The entire rack contains 36 containers where each container has 3.576 kg natural uranium metal depletion.

c. The third scenario

- The ground floor of each rack contains 2x4 containers, 4 containers each loaded with 2.373 kg UCaF₂ with 19.75% enrichment, and 4 other containers each loaded with 7.111 kg metal Uranium with 19.75% enrichment.
- The first rack contain 3 shelves, each shelf contains 6 containers and each container containing 1.273 kg of natural UO₂. The entire first rack consists of 18 containers.
- The second rack contain 3 shelves, each shelf contains 6 containers and each container containing 3.576 kg of natural uranium metal depletion. The entire second rack consists of 18 containers.

Storage Facility 2

Storage facility 2 was designed to contain 2 storage racks that separated by a distance of 1m. Each storage rack comprises of a base and two levels of shelves.

The ground floor of each shelf hold 2 x 4 pieces of containers and each container has 30 cm diameter and 70 cm high. On the first and the second shelf were loaded with 2.373 kg UCaF₂ with 0.7% enrichment and 7.111 kg uranium metal with 0.7% enrichment. Each container was 50 cm apart from each other.

Furthermore, each level consists of a rack 2×4 containers. The diameter and height of each container is 30 cm and 34 cm respectively. Each container as far apart as 50 cm and containers made of iron.

- a. The first scenario
- The ground floor contains 2x4 container, 4 containers were loaded with 2.373 kg UCaF₂ with 19.75% enrichment, and 4 other containers loaded with 7.111 kg metal Uranium with 19.75% enrichment.
- The first rack and a second rack consist of 2 shelves. Each shelf contains of 4 containers. The entire racks contain of 16 containers, each container has 0.106 kg of natural U_3O_8 .

b. The second scenario

- The ground floor contains 2x4 container, 4 containers were loaded with 2.373 kg UCaF₂ with 19.75% enrichment, and 4 other containers loaded with 7.111 kg metal Uranium with 19.75% enrichment.
- The first rack and a second rack each consisting of 2 shelves. Each shelf contains of 4 containers. The entire racks contain of 16 containers, each container has 18.418 kg of natural UF_{4} .

c. The third scenario

- The ground floor of each rack of 2x4 containers, 4 containers each charged UCaF₂ mass of 2.373 kg with 19.75% enrichment, and 4 other containers each charged metal Uranium enrichment mass of 7.111 kg with 19.75%.
- The first rack consists of 2 shelves. Each shelf contains of 4 containers. The entire racks contain of 8 containers, each container has 0.106 kg of natural U_3O_8
- The second rack consisits 2 shelves. Each shelf contains of 4 containers. The entire racks contain of 8 containers, each container has 18.418 kg of natural UF₄.

Storage Facility 3

Storage facility 3 was designed to contain 2 storage racks that separated by a distance of 1 m. Each storage rack is consisting of the base and 3 levels of shelves.

The ground floor of each shelf was containing 3 x 6 pieces of container and each container of 30 cm diameter and 70 cm high. The container which is located on the ground floor, on the first shelf and the second shelf were loaded with UCaF₂ with mass of 2,373 kg with 19.75% enrichment and 7.111 kg uranium metal with 19.75% enrichment. Each container was 50 cm apart from each other.

Furthermore, every shelf level consists of (3×6) containers. Containers at the entire shelves have 14 cm in diameter and 17 cm high. Each container is separated by 39.5 cm and containers made of iron.

The first scenario

- The ground floor contains 2x4 containers, 4 containers each loaded with 2,373 kg UCaF₂ with 19.75% enrichment, and 4 other containers each loaded with 7.111 kg metal Uranium with 19.75% enrichment.
- The first rack and a second rack each consisting of three shelves: the first shelf to the third shelf, where every shelf contains 6 containers. The entire rack contains 36 containers with each container has 5.337 kg of $U_3 \text{Si}_2$ 19.75% enrichment.

RESULTS AND DISCUSSION

CELL MODEL FOR URANIUM

In Figure 1, it is shown in the left-hand side the model for a front view of the container, while the right image is modeling for top view of the container. Red color indicates a material homogenization of uranium materials inside the container and blue is the homogenization of the material contained.



Figure 1. The cell model for uranium materials

SYSTEM MODEL FOR THREE STORAGE FACILITIES

1. System Model for Initial Condition Storage Facility

Sorage Facility 1

Figure 2 in the left hand-side shows the image model of the view from the front, while in the right-hand side shows a view from above. Figure 2 represents the material uranium only in one level and consists of two types (natural UO_2 and depleted uranium metal), and each type consisting of 2x5 container.

	aface Cell Seurce Data Run ParticleDeplay Ta	By Plate Cross section plots 30 W	ev CAD import Read_age	n Backap Vieb	alte Optiere	New 1980				
Land City	Der Konnen IV Der Konne Frisken Mehren Konne Frisken Jereit (10 m. 10 Jereit (10 m. 10 Jereit (10 m. 10) Jereit (10 m. 10	1 4000 (1 4000 (1 4000 2011 h	North Carlos	(inter er) Unter (d), Dem st	er Politice (C NENEC (Data	• p	i v i i i i i i i i i i i i i i i i i i	.000 [9 1.000	ja ja žom is	
289 289			10 10 10 10 10 10 10 20 20 20 20 20 20 20 20 20 2		Θ	Θ	Θ	Θ	Θ	1
			Call for a		⊖ ●	<i>⊡</i>	•	<i>⊡</i>	<i>⊡</i>	
			And do		•	•	•	•	•	j

Figure 2. System model for a storage facility 1 in the current condition

Storage Facility 2

Figure 3 depicts the view from the front (left-hand side), whiles the image to the righthand side, and shows a view from above. Figure 3 represents material uranium only in one level and consists of two types (natural UO_2 and $UCaF_2$), and each type is composed of five containers.

NO PX	Tisual Ecîter Versia	n X_225 - 1: 1	WOPK	illalitesWesterSc									- C X
1: D.V	CHPWritikalitasW	esus5c	a han haro	оеоодау тақию	s tras secondos		2: 0.V	ANE ⁿ Kritika	itanWarunS	c vev			
laters Level	Dead v 0 Later: CO. v Zoon out	[[620.3200] [46	4280 [12 Level		2000 0 1.0000 Zoan in		Update Last Sirc Repet	United CEL Zoon aut	AU 846 (9	K.6082 J	• 11	1.0000 0 0 1.0000	0 9 - Zoon is
C Osph							Dans Days 						
							-13 Grave -1539 -1539			~			
Dates							Granten		_	_	•		
D Case D Fanas Waltain Cell Dro w							Ger Color Ger Facetor With Watch Cell Libre w	•		•	•	•	•
Field Taimeth Robert about Anial 15							Flat mesh Retain about Area 10						
VAL 10 Hall 10 For state w													
Pauge	PX Visual Edit	or MCI	VPX Visi	ual Editor	MCNPX V	isual Edi	Product	MCNPX 1	isual Ed	itor i	MCNPX Vis	ual Editor	MCNPX Vis
	000	a colator						- - H24	W Vousi Ed	D Lands	- Internal - 20	e a tiére	1080 osan

Figure 3. System model for storage facility 2 in current condition

Storage Facility 3

Figure 4 shows for the image model of the view from the front (left-hand side), while the model image to the right, shows a view from above. Figure 4 represents the material uranium only in one level and consists of two types (natural $UCaF_2$ and uranium metal), and each consisting of 4x5 container types.

MONEX	risual Editer Tension X, 225 - 1: D;WCNPWritkatilasWasas6d	In second second		a factor	and the	Castless - Ma					
-ee 2464X	Uppering survey of survey bits was harder basis to the host crisis debas parts so the C Uppering the Des Survey of the host crisis debas parts so the C	2 D 10	IO PI	n Babap Kritikalit	moccas es VCes un 6	options we	n NGD				
Lat ford	Solution -107 /r00 00 00 /r0714 102 0<	Update Last Sect	Got	6 . [00.	C41630 8 ▼	5766 0	Level:		000 0	0	
Zon	Jimite j John	Tana Zon	am								
12		18									
_0 Doubt		-lo Dees									
220		_200 _200									•
Retreat		Fathsh									•
Color		Cel 16	ŀ								
W Fands MW MpA		Cel Une w						-	-	<u> </u>	<u> </u>
Rat		Fact									•
Anial 10		Forge about									•
Ver 15 Note 15		Ver 15 Rott 15									
ne posle 💌 Real 300		NO JEAN W									
E Print		E Prospi									

Figure 4. System model for the storage facility 3 in current condition

2. System Model with Storage Racks

Storage Facility 1

Figure 5 shows the first rack, which is represented by models 1 (front view) and 2 (side view), and the second rack, which is represented by models 3 (front view) and 4 (side view). It is shown in Figure 5 also that uranium materials at a lower shelf consist of 2 uranium types (UCaF₂ and uranium metal). Each shelf consisted of four containers. In the entire three shelves consists of one type of uranium (UO₂/uranium metal), and was simulated into three scenarios. Scenario 1: the entire racks consist of UO₂ and contain 36 containers. Scenario 2: the entire first rack consists of UO₂ (18 containers) and the entire second rack consists of ranium metal (18 containers).



Figure 5. System model for storage facility 1 with first and second racks

Storage Facility 2

Figure 6 depicts the first rack, which is represented by models 1 (front view) and 2 (side view), and the second rack, which is represented by models 3 (front view) and 4 (side view). It is also shown in Figure 5 that uranium materials at lower shelf consists of 2 uranium types (UCaF₂ and uranium metal). In the entire racks consists of one type of uranium (U₃O₈/UF₄), and

was simulated into three scenarios. Scenario 1: the entire racks consist of U_3O_8 and contain 16 containers. Scenario 2: The entire racks consist of UF₄ and contain 16 containers. Scenario 3: The entire first rack consists of U_3O_8 (8 containers) and the entire second rack consists of UF₄ (8 containers).



Figure 6. The system models the storage facility with the first rack and a second rack

Storage Facility 3

Figure 7 depicts the first rack, which is represented by models 1 (front view) and 2 (side view), and the second rack, which is represented by models 3 (front view) and 4 (side view). It is also shown in Figure 5 that uranium materials at lower shelf consists of 2 uranium types (UCaF₂ and uranium metal). On the third level rack consists of one type of material uranium (U₃Si₂), and simulated into one scenario that is the entire shelf in the entire rack consists U₃Si₂ in 36 containers.



Figure 7. The system models the third storage facility with the first rack and a second rack

Futhermore after all the model is defined, the calculation is carried to determine the volume fraction and the density of atoms for every material used in the storage facilities 1, 2 and 3 using the formula (4) to (11) and the results can be seen in Table 1, 2 and 3.

Material	Mass of Atom	Density (gram/cm ³)	Enrichment (%)	Mass (gram)	% Weight	Atomic Density
UO ₂	-	10.97	0.70	1273		-
U	237.45	11.3	-	-		-
U-235	235.04	-	-	-	0.007	1.28E-04
U-238	238.05	-	-	-	0.993	1.79E-02
Ο	16.00	-	-	-		2.44E-03
Ν	14.00	-		-		3.89E-10
С	12.00	-		-		5.63E-12
Plastic						

Table 1. Material input MCNP-5 for the initial condition of storage facilities 1

Material	Mass of	Density	Enrichment	Mass (gram)	% Waight	Atomic
	Atom	(gram/cm)	(70)	(grain)	weight	Delisity
C	12.00				0.8562	-
Н	1.01				0.1438	-
U metal	-	18.95	0.07	3576		-
U-235	235.04	-	-	-	0.007	6.14E-04
U-238	238.05	-	-	-	0.993	8.68E-02
Air	-	0.0012	-	-		-
С	12.00	-	-	-		7.45E-06
Ν	14.00	-	-	-		3.84E-05
Ο	16.00	-	-	-		1.03E-05
Ar	39.95	-	-	-		2.28R-07
Ne	20.17	-	-	-		4.24E-10
He	4.00	-	-	-		1.25E-10
Kr	83.78	-	-	-		2.55E-11
Н	1.01	-	-	-		4.19E-13
Xe	131.26	-	-	-		2.17E-12

Table 1 shows that the material, which can be stored in Storage Facility 1 are OU_2 with 1273 gr mass and Uranium Metal with 3576 gr mass. Two uranium types, which will be placed in container, are built from plastic material. OU_2 material consists of 1.28E-04 atom/cm³ of U-235 and 7.21E-03 atom/cm³ of U-238 and uranium metal consists of 6.14E-04 atom/cm³ of U-235 and 8.68E-02 atom/cm³ of U-238. This case shows that the U-235 mass in UO₂ and uranium metal material is very small compare to the U-238 mass. It is because the enrichment of uranium in UO₂ and uranium metal is quite small at 0.7%. It also shows that the number of U-235 in uranium metal more than in UO₂, this is because the uranium metal mass is greater than the UO₂ mass.

Table 2. Material	input MCNP-5	for initial	conidition	of storage	facilities 2
1 uoio 2. muteriu	imput morti 5	ioi iiiitiui	configuration	or storage	iucilities 2

	Atomic	Density	Enrichmnt	Mass	%	Atomic
Material	weight	(gram/cm ³)	(%)	(gram)	Weight	Density
U ₃ O ₈	_	8.30	0.70	106	-	-
U	237.45	11.3	-	-	-	-
U-235	235.04	-	-	-	-	1.49E-06
U-238	238.05	-	-	-	-	5.98E-06
О	16.00	-	-	-	-	2.19E-04
Ν	14.00	-		-	-	8.41E-06
С	12.00	-		-	-	1.21E-05
Container						
Fe	55.84	7.87	-	-	-	-
UF_4	-	6.70	0.70	18984		-
U-235	235.04	-	-	-	0.007	1.04E-05
U-238	238.05	-	-	-	0.993	1.46E-03
F	19.00	-	-	-	-	5.87E-03
С	12.00	-	-	-	-	4.81E-08
О	16.00	-	-	-	-	1.13E-08
Ν	14.00	-	-	-	-	6.96E-10
Air	-	0.0012	-	-	-	-
С	12.00	-	-	-	-	7.45E-06
Ν	14.00	-	-	-	-	3.84E-05
О	16.00	-	-	-	-	1.03E-05
Ar	39.95	-	-	-	-	2.28R-07
Ne	20.17	-	-	-	-	4.24E-10
He	4.00	-	-	-	-	1.25E-10
Kr	83.78	-	-	-	-	2.55E-11
Н	1.01	-	-	-	-	4.19E-13
Xe	131.26	-	-	-	-	2.17E-12

Table 2 shows that the material, which can be stored in Storage Facility 1, are O_3U_8 with 106 gr mass and UF₄ with 18418 gr mass. Two uranium types, which will be placed in container, is built from plastic material. O_3U_8 material consists of 1.49E-06 atom/cm³ of U-235 and 5.98E-06 atom/cm³ of U-238. While UF₄ material consists of 1.04E-05 atom/cm³ of U-235 and 1.46E-03 atom/cm³ of U-238. It also shows that the mass of U-235 on UF₄ is greater than U₃O₈, this is due to the enrichment of both materials is the same, but the mass of UF₄ has greater than the mass of U₃O₈.

Material	Atomic weight	Density (gram/cm ³)	Enrichment (%)	Mass (gram)	% Weight	Atomic Density
U_3Si_2	-	12.20	19.75	5337		-
U	237.45	11.3	-	-		-
U-235	235.04	-	-	-	0.1975	4.24E-03
U-238	238.05	-	-	-	0.8125	1.70E-02
Si	28.08	-	-	-		1.67E-03
Ο	16.00	-	-	-		8.21E-11
Ν	14.00	-		-		3.50E-10
С	12.00	-		-		5.06E-12
Container						
Fe	55.84	7.87	-	-	-	-
Air	-	0.0012	-	-	-	-
С	12.00	-	-	-	-	7.45E-06
Ν	14.00	-	-	-	-	3.84E-05
0	16.00	-	-	-	-	1.03E-05
Ar	39.95	-	-	-	-	2.28R-07
Ne	20.17	-	-	-	-	4.24E-10
He	4.00	-	-	-	-	1.25E-10
Kr	83.78	-	-	-	-	2.55E-11
Н	1.01	-	-	-	-	4.19E-13
Xe	131.26	-	-	-	-	2.17E-12

Table 3. Material input MCNP-5 for initial condition of storage facilities 3

Table 3 shows that the material, which can be stored in Storage Facility 1, is O_3Si_2 with 5337 gr mass. Only once uranium types, which will be placed in container, is built from iron. O_3Si_2 material consists of 4.24E-03 atom/cm³ of U-235 and 1.70E-02 atom/cm³ of U-238. Mass of U-235 in U_3Si_2 material has a large number, because the enrichment and mass of U_3Si_2 has a great values are 19.75% and 5330 grams respectively.

Of the three existing storage facilities, it is seen that the mass of uranium in each container in storage facility 3 is the largest U-235 mass compared to those in the storage facilities 1 and 2. The large amount of U-235 will generate a large probability of fission reactions, so that a critical condition will occurs sooner. Therefore forming material in the storage facilities 3 should be more attention.

Further calculation is aimed to obtain the level of criticality of the storage facility 1 to 3. The results obtained are presented in Table 4 to Table 6.

Table 4. Criticality level in storage facility 1

No.	Scenario	K-eff
1	Initial current condition	0.48171 ± 0.00155
2	First scenario	0.55478 ± 0.00123
3	Second scenario	0.55553 ± 0.00128
4	Third scenario	$\begin{array}{l} (0.55478 \leq \text{k-eff} \leq \ 0.55553) \\ \pm \ 0.00128 \end{array}$

Table 4 shows that at the initial state, the storage facility 1 is in sub-critical condition (k-eff = 0.48171 ± 0.00155). Condition storage facility 1 is safe because it is very far from the critical condition (k-eff = 1). Table 4 also shows that the storage facility 1 remains sub-critical after adding

2 storage shelves. The largest sub-critical condition is reached when the entire storage racks filled with depleted uranium metal container as many as 36 pieces (k-eff = 0.55553 ± 0.00128).

No.	Scenario	k-eff
1	Initial current condition	0.12443 ± 0.00026
2	First scenario	0.56036 ± 0.00134
3	Second scenario	0.50841 ± 0.00117
4	Third scenario	$(0.50841 \le \text{k-eff} \le 0.56036) \pm 0.00134$

Table 5. Criticality level in storage facility 2

From Table 5, it appears that the initial conditions of the storage facility are also sub-critical (k-eff= 0.12443 ± 0.00026). Of the three scenarios fuel storage in the storage rack, the largest criticality condition is reached in the second shelf, which is filled with U3O8 as many as 16 containers (k-eff= 0.56036 ± 0.00134).

No.	Scenario	k-eff						
1	Initial current condition	0.72995 ± 0.00166						
2	First scenario	0.96509 ± 0.00132						

Table 6. Criticality level in storage facility 3

Table 6 shows that the initial condition at the storage facility 3 is in the sub-critical condition with k-eff= (0.72995 ± 0.00166) . Subcritical stay remains after the entire shelf filled with U₃Si₂ as many as 36 containers with k-eff= 0.96509 ± 0.00132 .

Based on Table 4 to Table 6, it can be seen that the largest sub-critical condition in the storage facility 3. Based on the results it can be concluded that the entire three storage facilities in sub-critical conditions even with additional storage racks.

The fuel storage management was made based on the results. The goal of the management is so that each container position can be known in the storage area as well as the amounts of uranium inside the container is traceable. Uranium stoprage facility system management is accomplished through numbering the storage facilities. The container numbering is proposed as follows:

Container Number = FN-D/RM-YX

where:

- F = Storage fasility
- N = Storage fasility 1/2/3
- D/R = Ground/Rack
- M = Base or Rack 1/2
- Y = Front view of the foremost 1/2/3
- X = Side view of the leftmost. 1/2/3/4/5/6

Example:

A container is in storage facility 2. an place on the second rack in position number 2 from the front and the third from the left. For this condition the Number of container is namely **F2-R2-23** Monitoring Cards here after is devised to monitor the container as well as materials such in Tabel 7.

Container Number: F2-R2-23								
No.	Date	Type of Uranium	Initial Mass (Kg)	Addition Mass (kg)	Taken-out Mass (kg)	End Condition Mass (Kg)	Name/ sign	
1	02/01/17	U_3O_8	5.50	-	-	5.50		
2	10/03/17	U_3O_8	5.50	2.75	-	8.25		
3	15/03/17	U_3O_8	8.25	-	1.00	7.25		

Table 7. Card monitoring uranium materials

With the monitoring card as seen in Table 7, each container and its contents can be monitored and traced the amount of uranium that exists, and it history when added, retrieved, and is done by anyone. Thus it will be avoided uranium discharge to place unwanted and which will be hazardoues to workers, public and environtment because it is polluted by uranium.

CONCLUSION

The criticality Analysis of the storage facility has been completed. Criticality analysis results on the initial conditions for the three storage facilities are k-eff<1. As for the three storage facilities after the addition of storage racks resulted the lcriticality level in storage facilities 1,2 and 3 are also k-eff<1. All the storage facilities in a safe condition where k-eff values still far from critical condition at a price of k-eff = 1.00. The results are then used as the basis for the uranium materials management. The uranium material storage management based on the analysis was created to monitor the uranium material from traceability and illicit trafficking. Apart from that, the analysis results can be used as the basis to get the license of uranium material management from the regulatory body (BAPETEN).

ACKNOWLEDGEMENT

This research funded by PTKRN DIPA budget for fiscal year 2015. Our gratitude goes to the Head of PTKRN for use the DIPA budget. Thanks are also extended to colleagues Dr. M. Budi Setiawan from PTKRN-BATAN and Dr. Ing. Kusnanto from PT. INUKI (Persero) who helped researchers make this research done successfully.

REFERENCES

- 1. X-5 Monte Carlo Team *MCNP A General Monte Carlo N-Particle Transport Code, Version 5.* Los Alamos Nuclear Laboratory. Los Alamos - USA: 2005.
- Kastanya D. Critical mass calculations using MCNP: An academic exercise. Ann. Nucl. Energy. 2015. 75:228–231.
- Alloni D., Borio Di Tigliole A., Cammi A., Chiesa D., Clemenza M., Magrotti G., et al. Final characterization of the first critical configuration for the TRIGA Mark II reactor of the University of Pavia using the Monte Carlo code MCNP. Prog. Nucl. Energy. 2014. 74:129–135.
- 4. Robinson M.L., DeBey T.M., Higginbotham J.F. Benchmarking criticality analysis of TRIGA fuel storage racks. Appl. Radiat. Isot. 2017. **119**:16–22.
- 5. Wang M.-J., Sheu R.-J., Peir J.-J., Liang J.-H. Criticality calculations of the HTR-10 pebble-bed reactor with SCALE6/CSAS6 and MCNP5. Ann. Nucl. Energy. 2014. **64**:1–7.
- 6. Wang M.-J., Peir J.-J., Sheu R.-J., Liang J.-H. Effects of geometry homogenization on the HTR-10 criticality calculations. Nucl. Eng. Des. 2014. **271**:356–360.
- Setiawati E., Oktajianto H., Richardina V., Endro S J. Analysis loading height of HTR (High Temperature Reactor) core to obtain criticality of reactor. Int. J. Sci. Eng. 2015. 9:113–116.
- 8. Oktajianto H., Setiawati E., Richardina V. Modelling of HTR (High Temperature Reactor) Pebble-Bed 10 MW to determine criticality as a variations of enrichment and radius of the Fuel (Kernel) with the Monte Carlo code MCNP4C. Int. J. Sci. Eng. 2015. **8**:42–46.
- 9. Ho H.Q., Honda Y., Goto M., Takada S. Numerical investigation of the Random Arrangement Effect of coated fuel particles on the Criticality of HTTR fuel compact using MCNP6. Ann. Nucl. Energy. 2017. **103**:114–121.
- 10. Zuhair, Suwoto, Irianto I.D. Pemodelan teras untuk analisis perhitungan konstanta multiplikasi reaktor HTR-PROTEUS. Tri Dasa Mega. 2010. **12**(2):91–102.

- 11. Sudarmono, Suwoto, Hery A. Sensitivitas pengayaan dan fraksi packing partikel triso dalam bahan bakar Pebble terhadap k-inf sebagai dasar disain konseptual RGTT200K. J. Ilmu Daur Bahan Bakar Nuklir URANIA. 2013. **19**:25–38.
- 12. Odoi H.C., Akaho E.H.K., Jonah S.A., Abrefah R.G., Ibrahim V.Y., Al E.T. Study of criticality safety and neutronic Performance for a 348-Fuel-Pin Ghana Research Reactor-1 LEU core using MCNP code. World J. Nucl. Sci. Technol. 2014. 4:46–52.
- 13. Mosteller R. Comparison of ENDF / B-VII . 1 and ENDF / B-VII . 0 results for the expanded criticality validation suite for MCNP and for selected additional criticality benchmarks. Nucl. Data Sheets. 2014. **118**:442–445.
- 14. Zerovnik G., Podvratnik M., Snoj L. On normalization of fluxes and reaction rate in MCNP criticality calculation. Ann. Nucl. Energy. 2014. **63**:126–128.
- Hughes C.R., Pelaez O., Schubring D., Jordan K.A. Multi-physics analysis of a supercritical water reactor with improved MCNP modeling. Nucl. Eng. Des. 2014. 270:412–420.
- 16. NUKEM GMBH, Basic and Detail Engineering Process element fabrication plan for Badan Tenaga Atom Nasional *NUKEM VT-No 2.008*, HANAU, Germany, 1983